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Production and Depletion Calculations using MCNP

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Introduction: Codes for Time-Dependent Isotopic Evolution

- Isotope Generation and Depletion
 - ORIGEN-S/ORIGEN2 (ORNL) Matrix Exponential Method
 - CINDER90 (LANL) Markovian Chains
- Depletion codes require accurate cross section and flux data
 - MCNP provides system-dependent, energy-integrated cross sections/fluxes for important isotopes
 - MCNP links to CINDER90 internally or externally through *Monteburns* to any of the 3 codes in bullet 1
 - Activation script exists for proton irradiation of a target/spallation product generation
- Deterministic Lattice Physics Methods
 - CASMO/SIMULATE nodal 3-D simulator
 - Vendor Codes





Calculations Rely on Data

- Extent of Nuclides
 - CINDER90 3400 Isotopes, 1325 Fission Products
 - ORIGEN2 1700 isotopes, 850 Fission Products
 - ORIGEN-S 1946 isotopes, 1119 Fission Products
 - Applications such as radiochemistry are limited to ~40 nuclides; could benefit from more detailed calculations.

The blue isotopes

are all created by fission and decay

147La

¹⁴⁷Ba

into ¹⁴⁷Nd.

¹⁴⁷Ce

147Nd

¹⁴⁷Pr

- Fission Product Yields
 - ORIGEN includes up to 8 actinides/reactor type
 - CINDER90 includes up to 24 actinides from ENDF-B VI
 - Thermal: 18 isotopes, Fast: 22 isotopes,
 - 14 MeV: 11 isotopes, Spontaneous Fission: 9 isotopes



CINDER90 (Tal England, Bill Wilson)

- CINDER90 constructs sequences/chains of nuclide interactions and follows all possibilities until they are smaller than a limiting value.
- Much data for the CINDER90 library came from the Evolved Netherlands ٠ Energy Research Foundation Activation File (ECNAF) but may also be calculated by ALICE or McGNASH. **Cross Sections:**
 - Spontaneous fission
 - Spallation product generation
 - Radionuclide hazards (Cat 3)
 - Delayed neutrons (purpose of initial link to MCNP) more
 - Ground state plus first and second isomeric state nuclides
 - Processed spectral data: υ , β^- , β^+ , γ +X-ray, α emission
 - 63-group default neutron cross sections for a Power Reactor; collapsed to 1-group for actual calculations
 - 25-group photon spectra



- Fission, (n,γ) ,
- $(n,\alpha), (n,t)$
- (n,2n), (n,3n)

Methodology: System-Dependent Depletion Process



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Burnup (BU) = Power*Time/Tons Heavy Metal

Non-Linear Problem

- The depletion equation uses timedependent fluxes, interaction rates, and number densities to determine inventories as a function of time.
 - Unfortunately, the time-dependent flux also is dependent on the time-dependent nuclide density, thus making the depletion equation NONLINEAR
- Reaction rates must be reevaluated as spectrum alters further calculations
 - More time intervals = More computational cost
- MCNP6 approximate reaction rates over time

Steady State Flux Calculation (Predictor – may be optional in Monteburns)

Time Dependant Number Density Calculation (Predictor)

New Steady State Flux Calculation (Corrector)

Time Dependant Number Density Calculation (Corrector)

Final Result Based on Average Behavior





Flux Normalization/Power

| $C = \frac{P}{k_{eff}}$ | *V *Qrec | $\phi = C * f4tally$ $P = Q_{rec} * \phi * \Sigma_f * V$ | |
|-------------------------|-------------|--|--|
| Р | = | thermal power, | |
| k _{eff} | = | effective multiplication factor, | |
| υ | = | average number of neutrons produced per fission | |
| | | = $fsrc/floss$ or $k_{eff} * src/floss$ ("nps" vs. "ksrc" definition), | |
| floss | = | weight of neutrons lost to fission (from MCNP), | |
| Src | = | weight of source neutrons (~1), | |
| fsrc | = | weight of source neutrons gained in fission, | |
| $\Sigma_{ m f}$ | = | the macroscopic fission cross section, | |
| V | = | volume of material, and | |
| arphi | = | neutron flux. | |





Recoverable Energy per Fission (Q_{rec})

$$Q_{recoverable} = Q_{prompt} + Q_{delayed} + (\overline{\nu}(E) - k_{eff}) * Q_{capture\gamma} - Q_{neutrino}$$

Emitted and recoverable energy for fission of U-235

- CINDER90 gives Q_{rec} for 36 actinides
- Prompt Q value is determined from ENDF or other sources.
 - File 1 MT 458
 - MCNP6 has data for ~23 actinides
 - Additional Q values desired!
- Delayed Q value may be estimated assuming local energy deposition
 - General 11% increase may be applied.
 - Total Q increases with BU as higher actinides build in.
 - 207 of 390 isotopes contain capture gamma data in ENDF VII.0; deposited gamma energy may be calculated.



| \wedge | |
|------------|--|
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| Form | Emitted Energy (MeV) | Recoverable Energy (Mev) |
|---------------------------|-------------------------|-----------------------------|
| Fission Fragments | 168 | 168 |
| Fission Product Decay | | |
| γ -rays | 8 | 8 |
| β-rays | 7 | 7 |
| neutrinos | 12 | |
| Prompt gamma rays | 7 | 7 |
| Fission neutrons (kinetic | | |
| energy) | 5 | 5 |
| Capture γ-rays | | 3-12 |
| Fotal | 207 | 198-207 |

Applications

- Modeling of Full Reactor Cores
- Radiochemistry diagnostic calculations and nuclear detonation simulations
- Nonproliferation: determination of Pu, fission products, and more from irradiated nuclear fuel
 - Varies with reactor type
 - Process-dependent
- Innovative Reactor Concepts/Fuel Cycles
- Accelerator-Driven Systems





MCNP Full Reactor Core Modeling

- With increased computing power and memory reduction techniques, we can now model individual pins in a Pressurized Water Reactor core using Monte Carlo burnup simulations.
- 6,447 fuel pins in 1/8th core geometry, 1 axial segment
- Desired future features:
 - Even more memory reduction
 - More tally flexibility for *Monteburns*.



1/4 Core Burnup Distribution (GWd/MTU) Cycle 1

5

4

4

3

2

2

Comparison to Destructive Analysis (DA)

- H.B. Robinson infinitely-reflected assembly simulation.
- Plutonium isotopics can be predicted within 2-4% of measured values.
- Better benchmark data is desirable:
 - DA for multiple pins across the assembly,
 - Detailed operating history, and
 - Information on surrounding assemblies.

% Error = 100%* (Calculated – Measured)/Measured

| | 1 | |
|-------|-------|-------|
| | MCNP6 | SCALE |
| U235 | -0.08 | 1.97 |
| U236 | 0.17 | 0.52 |
| U238 | -0.73 | -0.07 |
| Pu238 | -8.58 | -11 |
| Pu239 | -0.20 | 4.21 |
| Pu240 | 1.32 | 3.94 |
| Pu241 | -2.56 | -1.72 |
| Np237 | 1.58 | 1.46 |
| Tc99 | 7.79 | 14.1 |
| Cs137 | -2.45 | 0.42 |



New Albedo Boundary Capability Assists Ability to Match DA







Desired Future Work: Memory Limitations Increase with:

- Isotopes tracked
 - Fission Products
 - Decay Chains
- Reaction rates calculated



- The more reaction rates that are calculated, the larger the storage requirements.
- Only most probable reaction rates should be tracked.
- Time steps calculated
- Geometrical size
 - Physical problem size
 - Giant systems may endure large temperature and material density variations leading to complicated meshing procedures to accurately calculate spatial reaction rates





Irradiation Creates Fission Products and Isomers

- ENDF/B-VII has 323 non-actinides and 70 actinides that can be included in irradiation, ~220 FPs, 3 elements, and 9 metastable isotopes.
- TENDL provides ~2000 isotopes but has not been tested for burnup.
- Lumped fission products may increase accuracy.
 - Fission products lacking data could be lumped into a problemdependent material for particle transport.
 - Improved computational cost, but
 - Results are sensitive to choice of fission products.
 - Lumped cross sections would be burnup-dependent.
 - How do we determine what worth value is an acceptable cutoff for lumping?
- Isomer branching following capture currently uses established fractions but should be energy-dependent.





Calculating Number Density Error and Error Propagation

- Toshikazu Takeda, Naoki Hirokawa and Tomohiro Noda "*Estimation of Error Propagation in Monte-Carlo Burnup Calculations*" Journal of Nuclear Science and Technology, Vol 36, No. 9, September 1999.
- Number density in depletion calculation satisfies the following equation:
 - M(t) = burnup matrix of group collapsed reaction rates

• N(t) = number density
$$\frac{dN(t)}{dt} = M(t)N(t)$$

- If $N_0(t_0)$ is the true number density then $N(t_0) = N_0(t_0) + \delta N(t_0)$
- If $M_0(t_0)$ is the true reaction rate then $M(t_0) = M_0(t_0) + \delta M(t_0)$
- Then we have an equation to explain change in error of the number density as a function of time step: $\frac{d\delta N(t)}{dt} = M_0(t_0)\delta N(t) + \delta M(t_0)N_0(t)$

Optimization of Hardware/Parallelization

- Continuously improving hardware is always desired!
- Calculations with large numbers of materials possible using:
 - OpenMPI parallel processing implementation for both transport and depletion
 - Infiniband
 - Nodes with lots of memory (256 GB 16 cores), and SSDs for swap space
- Example of large problem run: 3,960 materials to burn, ~25 seconds per material
 - Serial mode, 3,960*25 seconds = ~ 27 hours per production/depletion calc.
 - Parallel mode with ~200 processors scales by ~200, thus 27 hours \rightarrow ~10 min.
- Ability to choose different machinefile (hostfile) for parallel run
 - MCNP has optimum curve for selection of number of CPUs in kcode calculation
 - Too many will slow down calculation in communication
 - For production/depletion want to use as many CPUs as possible



Conclusions/Areas of Improvement

- Monte Carlo burnup capability has made HUGE progress!
- Full nuclear core modeling with MCNP now possible with limited axial fidelity.
- Future Work
 - More memory reduction
 - Incorporate full isotope chains into a range of calculations
 - Increase in products given detailed geometry/fluxes
 - Lumped fission products
 - *Monteburns* would benefit from tally flexibility; internal MCNP burn capability avoids the necessity
 - Need Q_{rec} values for more actinides
 - Energy-dependent isomer branching ratios
 - Other predictor-corrector methods should be explored





Applications: Large Reactor Core Design

- Traditional technique: deterministic
 - Solve lots of smaller calculations to get average parameters to solve the larger calculation.
 - Fuel bundle calculation generates collapsed group constants for the full core solution.
 - Utilize collapsed group cross sections to run a large-scale nodal calculation of reactor behavior.
- Increases in computational power now improve calculations!
 - Time-dependent behavior of every fuel pin is important.
 - MCNP can handle detailed, complex geometry with continuous-energy data.









Data Requests

- Two categories - CINDER90
 - Fission Yields \rightarrow England/Rider Data is from 1992
 - Data only exists for 0.025 eV,500 KeV, and 14 MeV
 - Does better fission yield data, at more energies, exist?
 - Proton libraries for minor nuclides
 - There are no proton libraries in CINDER90 for minor nuclides... This is important for proton target based interrogation
 - MCNPX
 - Lack of photon production data
 - Examine Am-241 capture xn to improve Cm-242 prediction





Traditional Predictor-Corrector

MCNP6 Predictor-Corrector



Isomer Branching

- MCNPX 2.6.0 over predicted (n, γ) by Tallying total (n, γ)
- At ICAPP 2008 → "future focus... include ENDF/B File 9 MT 102 and File 10 in ACE..."
 - W. HAECK, B. Cochet, L. Aguiar,
 "Isomeric Branching Ratio Treatment for Neutron-Induced Reactions," *Trans ANS*, 103, pg 693-695 (2010) – Memory Increase



- Isomer Branching in MCNP
 - Less memory and faster! $(n, \gamma)_{Corrected} =$

$$= \left(1 - \frac{\left(\sigma_{n,\gamma^{*}} * \Phi\right)_{C}}{\left(\sigma_{n,\gamma} * \Phi\right)_{M}}\right) \times \left(\sigma_{n,\gamma} * \Phi\right)_{M}$$

1



